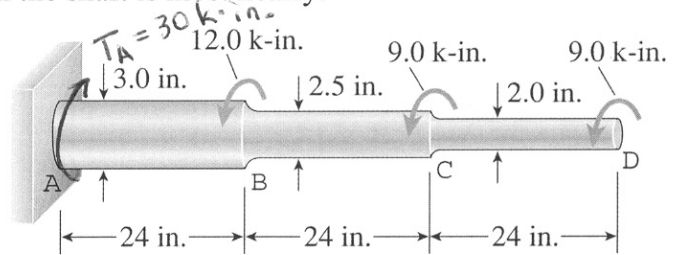


**MULTIPLE CHOICE PROBLEMS (10 Points each)**

1. A stepped shaft  $ABCD$  consisting of solid circular segments is subjected to three torques as shown in the Figure. The maximum shear stress,  $\tau_{\max}$ , in the shaft is most nearly:

- (a) 5.66 ksi
- (b) 5.87 ksi**
- (c) 733 psi
- (d) 5.73 ksi
- (e) 2.93 ksi



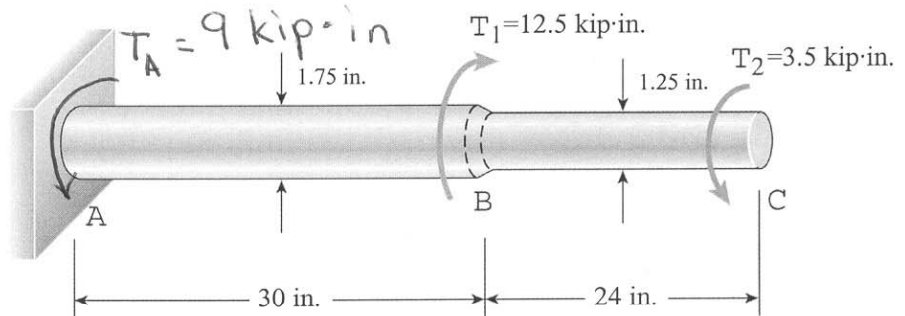
$$\tau_{AB} = \frac{T_{AB} r_{AB}}{J_{AB}} = \frac{T_{AB} r_{AB}}{\frac{\pi}{2} r_{AB}^4} = \frac{T_{AB}}{\frac{\pi}{2} r_{AB}^3} = \frac{30 \text{ kip}\cdot\text{in}}{\frac{\pi}{2} (1.5 \text{ in})^3} = 5.66 \text{ ksi}$$

$$\tau_{BC} = \frac{18 \text{ kip}\cdot\text{in}}{\frac{\pi}{2} (1.25 \text{ in})^3} = \underline{\underline{5.87 \text{ ksi}}}$$

$$\tau_{CD} = \frac{9 \text{ kip}\cdot\text{in}}{\frac{\pi}{2} (1 \text{ in})^3} = 5.73 \text{ ksi}$$

2. For the solid brass shaft shown,  $G = 17 \times 10^3$  ksi. The angle of rotation at section B is most nearly:

- (a)  $1.079 \times 10^{-3}$  radians
- (b)  $20.6 \times 10^{-3}$  radians
- (c)  $17.25 \times 10^{-3}$  radians**
- (d)  $24.0 \times 10^{-3}$  radians
- (e)  $73.7 \times 10^{-3}$  radians



$$\begin{aligned} \phi_B &= \phi_{B/A} = \frac{T_{AB} L_{AB}}{J_{AB} G} \\ &= \frac{(9 \text{ kip}\cdot\text{in})(30 \text{ in})}{\frac{\pi}{2} (0.875 \text{ in})^4 (17 \times 10^3 \text{ kip}/\text{in}^2)} \\ &= 0.01725 \text{ rad} \\ &= \underline{\underline{17.25 \times 10^{-3} \text{ rad}}} \end{aligned}$$

3. The flat bar shown has thickness 3.0 cm and fillets of radius  $R = 0.25$  cm. The larger width is  $b = 2.4$  cm and the smaller width is  $c = 1.6$  cm. It is subjected to a tensile load  $P$ . Determine the largest permissible load  $P$  if the maximum allowable normal stress in the bar is 20 MPa.

- (a) 4.92 kN  
 (b) 18.72 kN  
 (c) 6.27 kN  
 (d) 7.38 kN  
 (e) 17.47 kN

$$\frac{b}{c} = \frac{2.4 \text{ cm}}{1.6 \text{ cm}} = 1.5$$

$$\frac{R}{c} = \frac{0.25 \text{ cm}}{1.6 \text{ cm}} = 0.15625$$

$$\sigma_{\max} = K \sigma_{\text{ave nom}} = \sigma_{\text{all}}$$

$$\sigma_{\text{ave nom}} = \frac{\sigma_{\text{all}}}{K} = \frac{P_{\text{all}}}{ct}$$

$$P_{\text{all}} = \frac{\sigma_{\text{all}}}{K} ct$$

$$= \frac{20 \text{ N/mm}^2}{1.95} (16 \text{ mm})(30 \text{ mm}) = 4.92 \text{ kN}$$

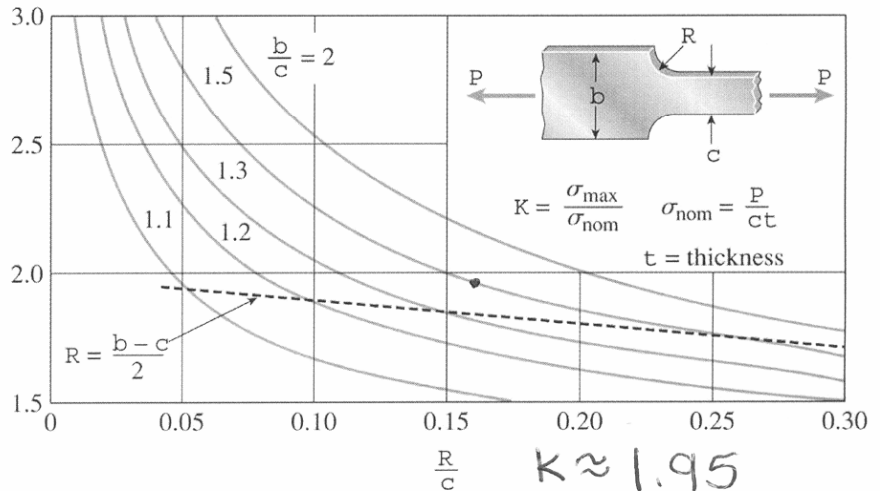
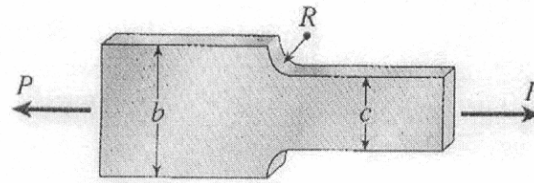
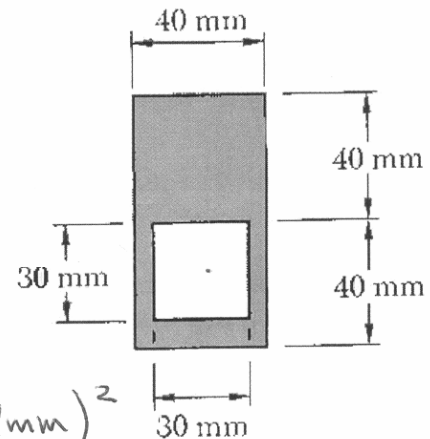


FIG. 2-64 Stress-concentration factor  $K$  for flat bars with shoulder fillets. The dashed line is for a full quarter-circular fillet.

4. The centroid of the section shown below is located 45.870 mm from the bottom of the area. The second moment of area (the area moment of inertia) about a horizontal axis that passes through the centroid of the area is most nearly:

- (a)  $4.27 \times 10^6 \text{ mm}^4$   
 (b)  $3.59 \times 10^6 \text{ mm}^4$   
 (c)  $1.357 \times 10^6 \text{ mm}^4$   
 (d)  $1.639 \times 10^6 \text{ mm}^4$   
 (e)  $1.707 \times 10^6 \text{ mm}^4$



$$I = \frac{1}{12} (80 \text{ mm})^3 (40 \text{ mm})$$

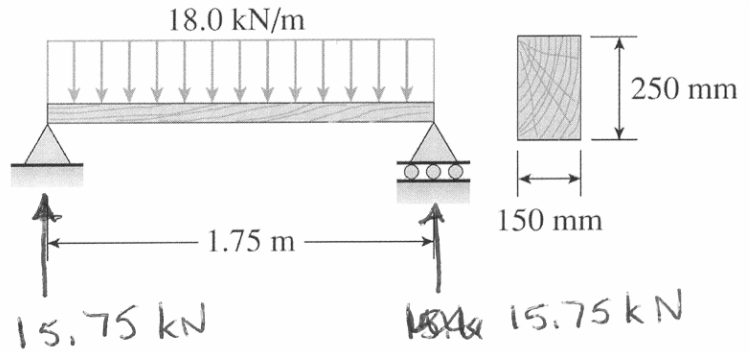
$$+ (80 \text{ mm})(40 \text{ mm}) (40 \text{ mm} - 45.87 \text{ mm})^2$$

$$- \left[ \frac{1}{12} (30 \text{ mm})^3 (30 \text{ mm}) + (30 \text{ mm})(30 \text{ mm}) (25 \text{ mm} - 45.87 \text{ mm})^2 \right]$$

$$= \underline{\underline{1.357 \times 10^6 \text{ mm}^4}}$$

5. The maximum bending stress in the simply supported wood beam loaded as shown below is most nearly:

- (a) 4.41 MPa  
 (b) 9.21 MPa  
 (c) 4.80 MPa  
 (d) 4.20 MPa  
 (e) 3.61 MPa



$$\sigma_m = \frac{M_{\max} c}{I}$$

$$= \frac{(6.89 \times 10^3 \text{ N}\cdot\text{m})(0.125 \text{ m})}{\frac{1}{12} (0.15 \text{ m})(0.25 \text{ m})^3}$$

$$= 4.41 \times 10^6 \text{ N/m}^2 = \underline{4.41 \text{ MPa}}$$

$$M_{\max} = \frac{1}{2} (15.75 \text{ kN})(0.875 \text{ m})$$

$$= 6.89 \text{ kN}\cdot\text{m}$$

6. Point A is deflected downward by a very small increment,  $\delta$ , in response to the load, P. The corresponding shear stress in rod BC which has a diameter  $d$  is given by:

(a)  $\tau_{\max} = \frac{G\delta a}{Ld}$

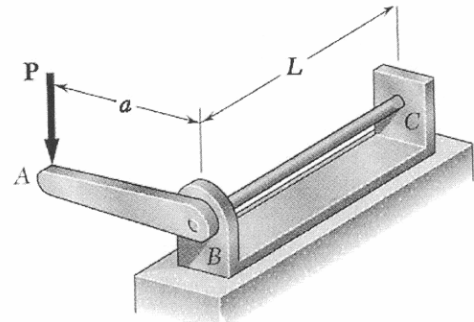
(b)  $\tau_{\max} = \frac{Gd\delta}{La}$

(c)  $\tau_{\max} = \frac{Gd\delta}{2La}$

(d)  $\tau_{\max} = \frac{G\delta a}{6Ld}$

(e)  $\tau_{\max} = \frac{d\delta a}{2GL}$

$$T = Pa$$



$$\phi_B = \phi_{B/C} = \frac{\delta}{a} = \frac{TL}{JG}$$

$$\frac{\delta}{a} \frac{JG}{L} = T$$

$$\tau_{\max} = \frac{Tc}{J} = \frac{\frac{\delta}{a} \frac{JG}{L} \left(\frac{d}{2}\right)}{J} = \frac{G\delta d}{2aL}$$

## 7. WORK OUT PROBLEM (40 Points)

Two solid steel shafts are fitted with rigid flanges which are then connected by fitted bolts so that there is no relative rotation between the flanges. Knowing that  $G = 77 \text{ GPa}$ , determine the maximum shearing stress in shaft AB when a torque of magnitude  $T = 500 \text{ N}\cdot\text{m}$  is applied to flange B.

Equilibrium:

$$T_A + T_D = T \Rightarrow T_D = T - T_A$$

Kinematics:

$$\phi_{B/A} = \phi_B = \phi_C = \phi_{C/D}$$

Torque - Angle of twist:

$$\phi_{B/A} = \frac{T_{AB} L_{AB}}{J_{AB} G} = \frac{T_A L_{AB}}{J_{AB} G}$$

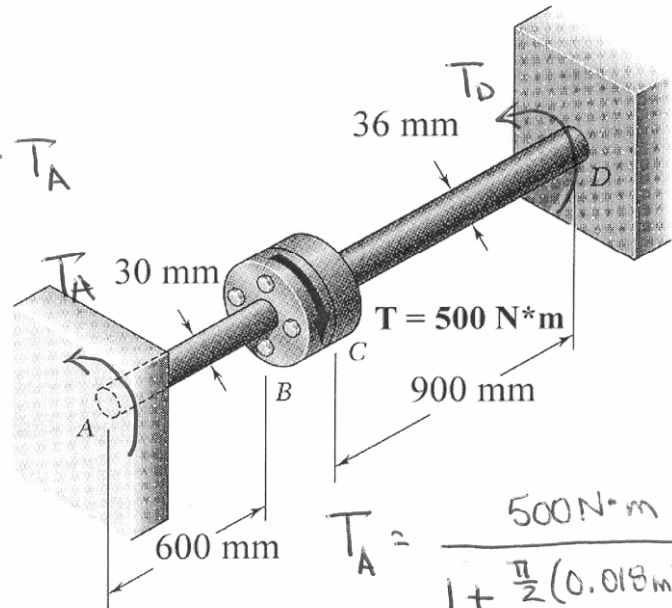
$$\phi_{C/D} = \frac{T_{CD} L_{CD}}{J_{CD} G} = \frac{T_D L_{CD}}{J_{CD} G}$$

$$\phi_{B/A} = \phi_{C/D} \Rightarrow \frac{T_D L_{CD}}{J_{CD} G} = \frac{T_A L_{AB}}{J_{AB} G}$$

$$\frac{(T - T_A) L_{CD}}{J_{CD} G} = \frac{T_A L_{AB}}{J_{AB} G}$$

$$\frac{T L_{CD}}{J_{CD} G} = T_A \left( \frac{L_{CD}}{J_{CD} G} + \frac{L_{AB}}{J_{AB} G} \right)$$

$$T_A = \frac{T L_{CD}}{J_{CD} G} / \left( \frac{L_{CD}}{J_{CD} G} + \frac{L_{AB}}{J_{AB} G} \right) = \frac{T}{\left( 1 + \frac{J_{CD} L_{AB}}{J_{AB} L_{CD}} \right)}$$



$$T_A = \frac{500 \text{ N}\cdot\text{m}}{1 + \frac{\frac{\pi}{2} (0.018 \text{ m})^4}{\frac{\pi}{2} (0.015 \text{ m})^4} \frac{600 \text{ m}}{900 \text{ m}}} = 210 \text{ N}\cdot\text{m}$$

$$T_{AB} = \frac{T_A L_{AB}}{J_{AB} G} = \frac{(210 \text{ N}\cdot\text{m}) (0.015 \text{ m})}{\frac{\pi}{2} (0.015 \text{ m})^4} = 39.6 \text{ MPa}$$